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### **Thermal shock behavior of $\text{Cr}_2\text{O}_3$ - based plasma sprayed coatings**

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**Abstract.** Atmospheric Plasma Spray (APS) coatings have earned a well-deserved place in the category of thermal spray coatings over the last decades, as they have brought coatings made of ceramic materials to the forefront. This has greatly extended the range of applications of these coatings, ranging from improved wear resistance to enhanced resistance to use at very high temperatures. In this study it is analyzed how two thermally sprayed  $\text{Cr}_2\text{O}_3$ -based coatings, a 99wt%  $\text{Cr}_2\text{O}_3$  powder and a  $\text{Cr}_2\text{O}_3$ -10wt% $\text{TiO}_2$  powder, were affected by exposure to thermal shock, with temperatures recorded in the range of 700 to 900°C. The samples were analyzed by scanning electron microscopy and EDS analysis (Energy Dispersive Spectroscopy), the results being completed by roughness measurements on the affected areas using a Mahr perthometer and AFM (Atomic Force Microscopy). No major changes were observed in the comparative behavior of the two coatings, nor in comparison with the material not affected by thermal shock, both in terms of morphology and chemical composition of the areas subjected to thermal shock, as well as their roughness or compactness. It can thus be concluded that the presence of a small percentage of  $\text{TiO}_2$  does not negatively influence the thermal shock behavior of this type of coating, and the range of applications can be extended to high temperatures.

**Keyword:** plasma spray, thermal shock, chromium oxide, coating morphology.

#### **1. Introduction**

One of the effective ways to improve the mechanical, physical and chemical properties is to modify material characteristics in the surface area, rather than modifying the entire material mass. Thus, through surface engineering, the service life can be extended by improving the mechanical characteristics of resistance to

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fatigue, wear, friction, or the physical, chemical and thermal characteristics of resistance to corrosion and high temperatures.

Surface engineering has a multitude of methods available for modifying interfaces, either by layer transformation with microstructure modification, or by coating with various types of layers, physicochemically or mechanically bonded to the substrate [1]. One method that has gained a lot of ground in the last decades is the deposition of thermal spray coatings [2]. This method is characterized by the formation of a coating with a lamellar structure that can have thicknesses ranging from 50 microns to a few millimeters and can be made of both metallic, but also ceramic or ceramometallic materials, single or combined in several successive layers [3].

One such layer is that obtained from a chromium oxide ceramic matrix, which can be deposited as such or combined with various other ceramic and/or metallic materials [4]. Cr<sub>2</sub>O<sub>3</sub> coatings have found numerous industrial applications over time, such as the protection of surfaces exposed to severe working conditions in the aerospace, energy, automotive, chemical and even food industries [5].

One of the most common applications is the protection against abrasive wear and erosion, even in abrasive fluids (slurry erosion). Cr<sub>2</sub>O<sub>3</sub> coatings are used in high-performance equipment such as press rollers in the printing industry, components subject to intense friction such as pistons and cylinders in internal combustion engines and in the aerospace industry [6, 7], providing effective protection and prolonging their service life. These coatings have high wear resistance due to their high hardness (above 1600 HV) as well as low coefficient of friction. A study [8] on the erosion behavior of Cr<sub>2</sub>O<sub>3</sub> layer applied on martensitic steel (AISI 410) showed that the impact angle of the eroding particles significantly influences the wear resistance, even at impact angles of 60° and 75°, compared to lower angles. In highly demanding industrial environments, such as mining facilities and hydropower equipment, Cr<sub>2</sub>O<sub>3</sub> coatings applied on metallic substrates protect against erosion and abrasion caused by suspended solid particles, an example being the study on Cr<sub>2</sub>O<sub>3</sub> coatings deposited on AISI 410 steel that provided superior resistance compared to uncoated substrates [9].

Cr<sub>2</sub>O<sub>3</sub> coatings are also known for their excellent corrosion resistance, which makes them suitable for applications where components are exposed to aggressive chemical or saline environments, such as turbines, pumps, chemical processing equipment or those in the food industry [10, 11]. These dense, hard coatings act as a protective barrier, preventing corrosive agents from penetrating the metal substrate.

Another use of these coatings is for applications where materials are subjected to high temperatures due to their thermal stability and resistance to oxidation. These coatings are applied on components in gas turbines and power generation equipment to prevent degradation caused by extreme temperatures and eroding particles [7, 9], and have been shown to outperform other oxides, such as Al<sub>2</sub>O<sub>3</sub>, due to its chemical stability and oxidation resistance.

In tribological property testing, Cr<sub>2</sub>O<sub>3</sub> coatings demonstrated excellent performance in reducing friction and wear in both dry and wet contact. In addition, the

introduction of oxide additions, such as  $\text{TiO}_2$  and  $\text{Al}_2\text{O}_3$ , can modify the tribological properties and microstructure of the coating, improving wear resistance and hardness, so that  $\text{Cr}_2\text{O}_3\text{-TiO}_2$  and  $\text{Cr}_2\text{O}_3\text{-Al}_2\text{O}_3$  coatings exhibit higher wear resistance in intense friction applications and provide high stability in high temperature environments and intense mechanical loads [12 - 14].

A disadvantage of  $\text{Cr}_2\text{O}_3$  coatings is their local brittleness, which manifests itself especially if they are subjected to very high local pressures during use [15], which generate macro-cracks and implicitly the destruction of the coating. A method to diminish this undesirable characteristic is the addition of oxides in the flow of spray material, such as  $\text{Al}_2\text{O}_3$  [16],  $\text{TiO}_2$  [17],  $\text{ZrO}_2$  [7],  $\text{BaCrO}_4$  [18] or  $\text{SiO}_2$  [19], both individually and in complex combinations. Their addition in small percentages (less than 5%wt) has the effect of forming glassy phases with low melting point, to increase the adhesion between the lamellae in the deposited layer without changing the intrinsic characteristics of the  $\text{Cr}_2\text{O}_3$  [7] matrix. Several low alloyed powders with  $\text{TiO}_2$ ,  $\text{ZrO}_2$  [7],  $\text{SiO}_2$  [24], or combinations thereof have already become commercial materials [13]. A series of nanostructured  $\text{Cr}_2\text{O}_3$  - Ag nanostructured coatings [20] are currently being tested to improve the structural characteristics and mechanical properties, and both the mechanisms of high temperature formation of the lubricant film on  $\text{NiCoCrAlY}$  -  $\text{Cr}_2\text{O}_3$  - AgMo coatings [21] and the effect of graphite addition [22] are being studied to improve the tribological characteristics.

According to the studies available in the literature, titanium oxide ( $\text{TiO}_2$ ) can significantly improve the properties of chromium oxide ( $\text{Cr}_2\text{O}_3$ ) coatings made by thermal spraying, influencing several key aspects related to mechanical strength, wear resistance and tribological behavior. In terms of toughness improvement and porosity reduction,  $\text{TiO}_2$  contributes to reduce the porosity of  $\text{Cr}_2\text{O}_3$  coatings and increase their density. This combination leads to improved mechanical strength and a more uniform particle distribution [22, 23]. In particular, the addition of  $\text{TiO}_2$  helps to reduce microcracking and improves the ability to withstand high mechanical loads [19, 24]. Other studies have shown that the inclusion of  $\text{TiO}_2$  in  $\text{Cr}_2\text{O}_3$  coatings improves wear and erosion resistance by reducing the tendency to microcracking and improving toughness [23, 24]. For example,  $\text{Cr}_2\text{O}_3\text{-25\%TiO}_2$  coatings have higher abrasion resistance, which makes them more suitable for applications in demanding environments such as industrial equipment [7, 22].

$\text{TiO}_2$  also acts as a solid lubricant in  $\text{Cr}_2\text{O}_3$  matrix coatings, which leads to a decrease in the coefficient of friction and improved tribological behavior under severe friction conditions [22, 24]. Another advantage of  $\text{Cr}_2\text{O}_3\text{-TiO}_2$ -based coatings is that they exhibit superior thermal stability of the constituent phases at elevated temperatures, as  $\text{TiO}_2$  intervenes in the formation of a stable solid solution in the crystalline structure of  $\text{Cr}_2\text{O}_3$ , thus preventing degradation of the material [7, 23], which can thus be used in applications involving exposure to high temperatures. In corrosive environments,  $\text{Cr}_2\text{O}_3\text{-TiO}_2$  coatings exhibit superior corrosion resistance compared to that of a coating made solely of  $\text{Cr}_2\text{O}_3$ , due to its denser structure and its protective properties against oxidation [19].

In this study, it was observed how two thermally sprayed Cr<sub>2</sub>O<sub>3</sub>-based coatings, a Cr<sub>2</sub>O<sub>3</sub> powder (99wt%) and a Cr<sub>2</sub>O<sub>3</sub>-10wt%TiO<sub>2</sub> powder, were affected by exposure to thermal shock, with temperatures recorded in the range of 700 to 900°C. The thermal shock was obtained by heating-cooling cycles exposure in a 2kw MSSf vertical axis solar furnace in the PROMES / CNRS laboratory in Odeillo - Font Romeu France. The samples were analyzed by scanning electron microscopy and EDS analysis (Energy Dispersive Spectroscopy), the results being completed by roughness measurements on the affected areas using a Mahr Perthometer and AFM (Atomic Force Microscopy).

## **2. Experiment**

### **2.1. Materials and methods used for APS coatings**

In order to study how the TiO<sub>2</sub> alloying percentage influences the microstructure of a plasma-spray deposited (APS) Cr<sub>2</sub>O<sub>3</sub>-based matrix coating, two commercially available powders were purchased from the market: Amdry 6415 (99%wt Cr<sub>2</sub>O<sub>3</sub>, melt sintered and ground) and Metco 6483 (40%wtTiO<sub>2</sub>, mixed). To modify the alloying percentage, the amounts required to obtain 10wt% TiO<sub>2</sub> alloying by mechanically mixing Cr<sub>2</sub>O<sub>3</sub> powder with Cr<sub>2</sub>O<sub>3</sub>-40%wtTiO<sub>2</sub> powder were calculated and measured by weighing on an electronic balance [25]. The nominal particle size distributions are (- 15 +5) µm for Cr<sub>2</sub>O<sub>3</sub> powder and (- 90 +16) µm for Cr<sub>2</sub>O<sub>3</sub>-40%wt%wt TiO<sub>2</sub>, both with an angular polygonal morphology.

The SprayWizard 9MCE (Metco - Oerlikon, 2006) was used for thermal spraying, with the following parameters: voltage - 58.8 V, current - 496 A, primary gas flow (argon) - 60 NLPM, secondary gas flow (hydrogen) - 45 NLPM, powder feed rate. The substrate is low alloy steel (max.0.17%C, max. 1.4%Mn, max. 0.035%P, max. 0.035%S, max. 0.12%N, max. 0.55%Cu, according to EN 10025-2/2004), with a rectangular geometry (60 x 30 x 5 mm) and rounded corners. The surface of each sample was prepared by sandblasting with quartz sand in order to clean all the impurities and activate it by texturizing. To ensure the reproducibility of the experiment, three samples of each type of coating were produced.

### **2.2. Materials and methods used for thermal shock study**

The study of the thermal shock behaviour of the analysed coatings was carried out using a vertical axis solar furnace in the PROMES / CNRS Laboratory in Odeillo-Font Romeu France, by heating-cooling cycles exposure in a 2kw MSSf vertical axis solar furnace.

The samples were subjected in turn to heating-cooling cycles at temperatures between 800 and 900°C, cooling being carried out with a jet of compressed air blown over the heated area. The temperature was recorded using a K-type thermocouple, some aspects during the tests being presented in Figure 3 a) - d). Figure 3 a) shows how the sample was mounted and the positioning of the K

thermocouple, which was connected to the Graphitec reader, that sequentially records the graph of the temperature variation over time (see Figure 4). Figure 3 b) shows the positioning of the sample under the concentrator. After that, a position of maximum concentration of solar radiation was obtained in an area higher than the sample surface, which was descended and stabilised on the sample surface (Figure 3 c). The thermal shock was obtained by periodically blowing jets of compressed air on the surface subjected to solar radiation, while blocking the heating.

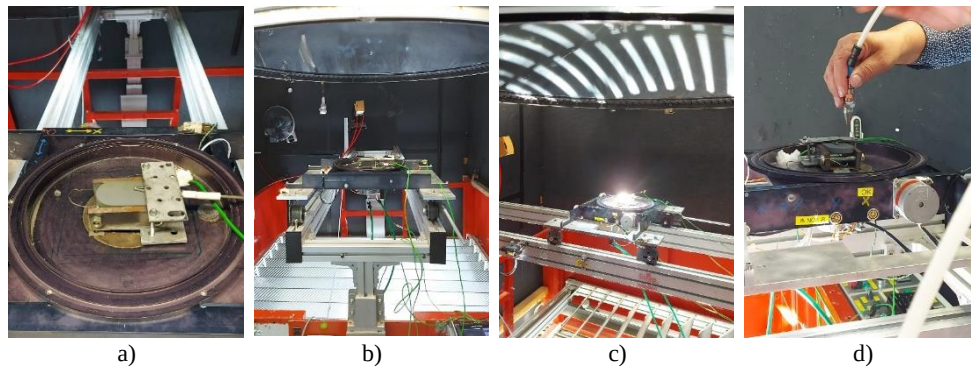


Fig. 3. Aspects during thermal shock tests: a) mounting of the sample and positioning of the K thermocouple, b) positioning of the sample under the solar concentrator, c) moment of positioning the focusing zone on the sample, d) forced cooling operation with compressed air for the thermal shock.

Figure 4 shows the 2 graphs generated during the heat shock tests for tested samples. The red line shows the temperature variation of the ceramic layer and the black line shows the temperature variation of the substrate.

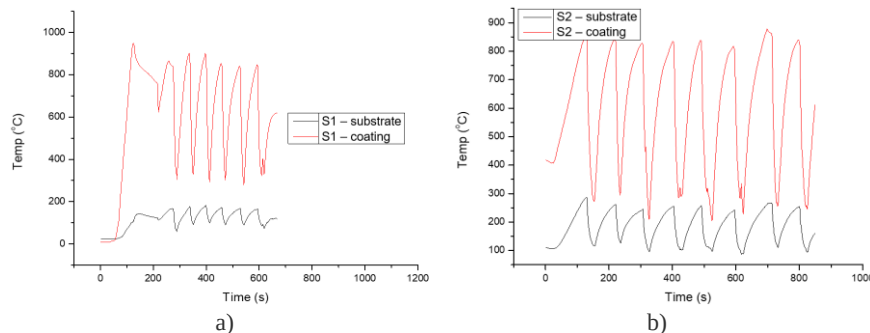


Fig. 4. Temperature variation graphs recorded during the thermal shock tests of: a) S1; b) S2.

It is observed that the temperature variations in the deposited layer are echoed in the substrate, but the temperature amplitude is small, which means that the substrate is not affected by major structural transformations.

The equipment used for the characterization of the layers subjected to thermal shock was the Vega Tescan II Scanning Electron Microscope and the EDS Detector produced by Bruker. An additional analysis of the surface roughness was

performed using Mahr Perthometer and Nanosurf Easy Scan 2 for Atomic Force Microscopy analysis.

### 3. Results and discussion

#### 3.1. SEM and EDS analysis of the S1 coatings (99%wt Cr<sub>2</sub>O<sub>3</sub>)

In the case of sample 1, it can be seen that no morphological change of the coatings occurs as shown in Figure 5, and the specific porous appearance of the thermal spray coatings is unchanged. However, a visible difference was observed in the form of color change ("staining") on the heat-affected area.

The elemental chemical analysis of the areas of interest did not show the presence of other elements, the distribution of Cr, O and C being uniform and unchanged compared to the initial reference area, as shown in Figures 6 and 7.

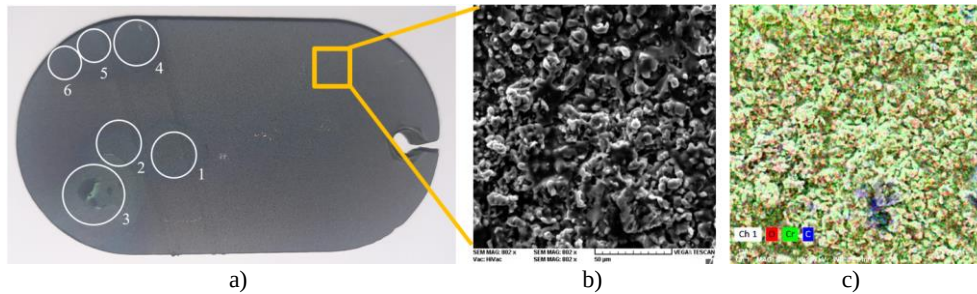


Fig. 5. The general aspect of sample 1 with areas subjected to thermal shock. Area of interest no.1: average temperature 800°C, 9 cycles/10 seconds

Fig. 6. Images of secondary electrons at 800 x (a) and EDS map at 500 x (b) on the reference surface of sample S1.

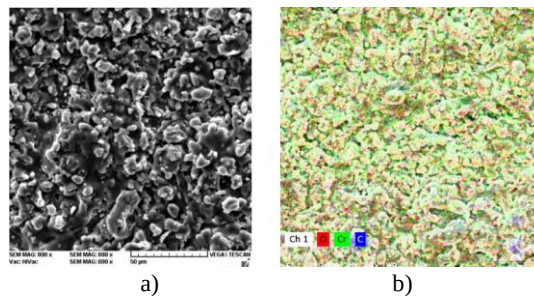


Fig. 7. Images of secondary electrons at 800x (a) and EDS map at 500x (b) on the thermal shock surface (area 1) of sample S1.

#### 3.2. SEM and EDS analysis of the S2 coatings (Cr<sub>2</sub>O<sub>3</sub> - 10%wt TiO<sub>2</sub>)

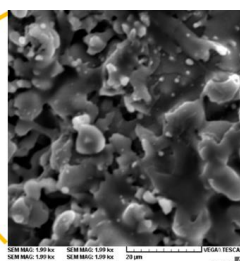
It can be seen that also in the case of sample 2 there were no changes in the morphology of the coating (e.g. local melting, oxidation with formation of oxide products, cracking) regardless of the temperature or cycles applied, as shown in the

Figures 8, 9 and 10. The same conclusion is supported by the distribution maps on the areas subjected to thermal shock, which show a uniform distribution of the component elements compared to the reference surface. The only changes, also in this case, are the darker patches on the heated areas, observed by visual analysis.

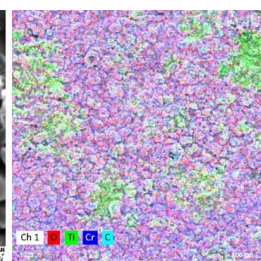


a)

Fig. 8. The general aspect of sample 2 with areas subjected to thermal shock. Area of interest no.4: average temperature 800°C, 9 cycles/10 seconds

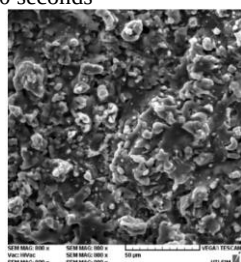


b)

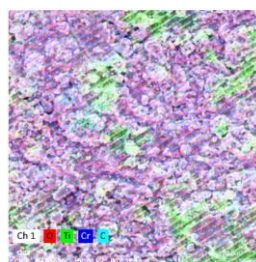


c)

Fig. 9. Images of secondary electrons at 2000x (a) and EDS map at 200x (b) on the reference surface of sample S2.



a)



b)

Fig. 10. Images of secondary electrons at 800x (a) and EDS map at 500x(b) on the thermal shock surface (area 4) of sample S2.

### 3.3. Comparative EDS analysis of the coatings after thermal shock

For an assessment of the degree of oxidation, the weight percentages of the chemical elements present in the areas subjected to thermal shock were comparatively analyzed and the values obtained are summarised in Table 1.

Table 1. Variation of the chemical elements percentage on the interest area of the samples subjected to thermal shock

| Sample                                                           | Area | %wt Cr | %wt O  | %wt Ti | %wt C |
|------------------------------------------------------------------|------|--------|--------|--------|-------|
| <b>S1 (99 wt% Cr<sub>2</sub>O<sub>3</sub>)</b>                   |      |        |        |        |       |
| Reference                                                        | 0    | 62.860 | 33.070 | -      | 4.060 |
| 800°C, 9 cycles x 10 sec.                                        | 1    | 64.760 | 32.930 | -      | 2.300 |
| <b>S2 (Cr<sub>2</sub>O<sub>3</sub> + 10 wt% TiO<sub>2</sub>)</b> |      |        |        |        |       |
| Reference                                                        | 0    | 49.930 | 38.940 | 8.610  | 2.520 |
| 800°C, 9 cycles x 10 sec.                                        | 4    | 49.340 | 39.430 | 7.660  | 3.570 |

It can be seen that there are no dramatic increases in the percentages of oxygen in any of the thermal shock areas compared to the reference areas (those on which no heat shock or heating was applied), so no additional oxidation of the layer occurs, regardless of the temperature at which it was heated.

However, there is a variation in the mass percentage of the chemical elements proportional to the change in the TiO<sub>2</sub> alloying percentage (as expected), namely: a decrease in the percentage of Cr with increasing TiO<sub>2</sub> alloying percentage and an increase in the percentages of Ti and O with increasing TiO<sub>2</sub> alloying percentage. A decrease in the percentage of C with increasing TiO<sub>2</sub> alloying is also observed.

### 3.4. Surface roughness evaluation after thermal shock – Mahr Perthometer

The surfaces of the areas subjected to thermal shock were also analyzed in terms of roughness variation, on each of the areas of interest, using a Mahr-type Perthometer. Three measurements were made for each area, the length of the route being the same for each case: Lt = 5.6 mm. The averaged values are summarised in Table 2.

When comparing the areas of each sample with the reference surface, no relevant changes in their roughness are observed. Also, when comparing the 2 types of coatings, it is observed that Ra increases slightly with increasing of the TiO<sub>2</sub> alloying percentage.

Table 2. Average values of the roughness of the interest areas of the samples subjected to thermal shock

| Sample                                                           | Area | Ra (avg)<br>[μm] | Rz (avg)<br>[μm] | Rmax (avg)<br>[μm] | Pc (avg)<br>[cm <sup>-1</sup> ] |
|------------------------------------------------------------------|------|------------------|------------------|--------------------|---------------------------------|
| <b>S1 (99 wt% Cr<sub>2</sub>O<sub>3</sub>)</b>                   |      |                  |                  |                    |                                 |
| <b>Reference</b>                                                 | 0    | 3.342            | 20.467           | 24.533             | 130.000                         |
| <b>800°C, 9 cycles x 10 sec.</b>                                 | 1    | 3.430            | 19.550           | 24.350             | 133.000                         |
| <b>S2 (Cr<sub>2</sub>O<sub>3</sub> + 10 wt% TiO<sub>2</sub>)</b> |      |                  |                  |                    |                                 |
| <b>Reference</b>                                                 | 0    | 4.419            | 27.400           | 37.167             | 86.000                          |
| <b>800°C, 9 cycles x 10 sec.</b>                                 | 4    | 3.830            | 24.400           | 32.250             | 124.000                         |

### 3.5. Surface roughness evaluation of the coatings after thermal shock (AFM)

Atomic force microscopy analysis was used for in-depth analysis of the influence of thermal shock on surface roughness at a micrometric scale, and thus on the structural transformations that might occur when thermal shock is applied.

For this reason, two surfaces were scanned on the areas of interest of sample 1, both on the reference surface (Figure 11) and on the surface affected by the thermal shock (Figure 12).



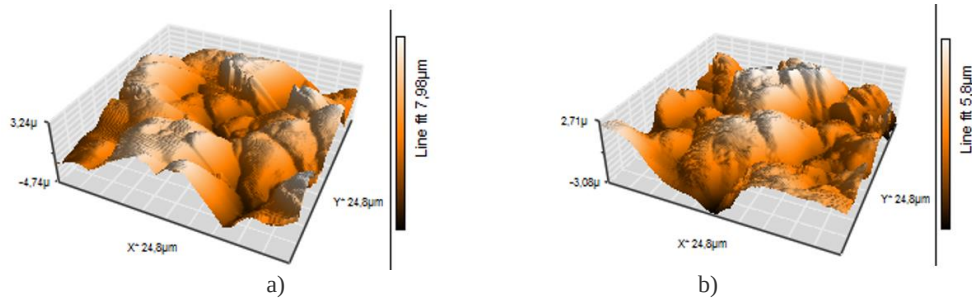


Fig. 11. 3D representations of the reference surface of sample 1: position 1 (a) and position 2 (b).

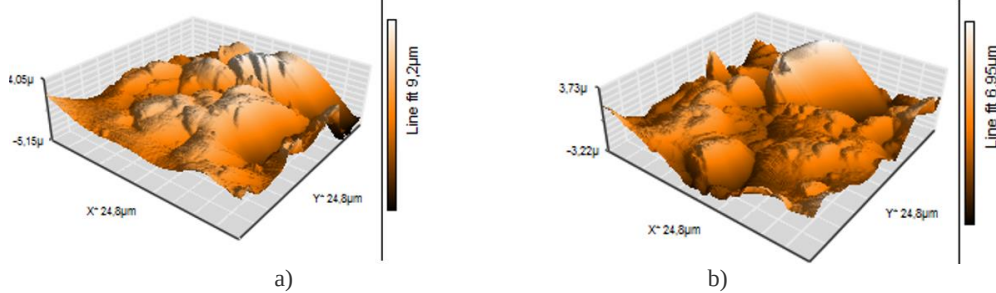


Fig. 12. 3D representations of thermal shock area no.1 from S1: position 1 (a) and position 2 (b).

Table 4. Roughness average values of the AFM scanned surfaces, from sample 1.

| Sample                                         | Area [ $\mu\text{m}^2$ ] | Sa [nm] | Sq [nm] | Sm [ $\mu\text{m}$ ] |
|------------------------------------------------|--------------------------|---------|---------|----------------------|
| <b>S1 (99 wt% Cr<sub>2</sub>O<sub>3</sub>)</b> |                          |         |         |                      |
| <b>Reference (1)</b>                           | 618                      | 1194.9  | 1408.9  | 342.99               |
| <b>Reference (2)</b>                           | 618                      | 919.61  | 1153.1  | 245.63               |
| <b>800°C, 9 cycles x 10 sec (1)</b>            | 618                      | 1239.5  | 1561.8  | 88.043               |
| <b>800°C, 9 cycles x 10 sec (2)</b>            | 618                      | 872.64  | 1114.1  | 273.17               |

In the resulting graphs, the irregular surface specific to thermal spray coatings can be seen. In the attached table (Table 4) the average values of the roughness of the scanned surface are presented, and it is observed that there is no clear trend of influence of the thermal shock application on the surface quality, at this scale.

The same observations were made for sample 2, as presented in Figures 13 and 14, so we cannot yet make clear comments on how the presence of TiO<sub>2</sub> influences the surface appearance of the samples before and after heat shock application.

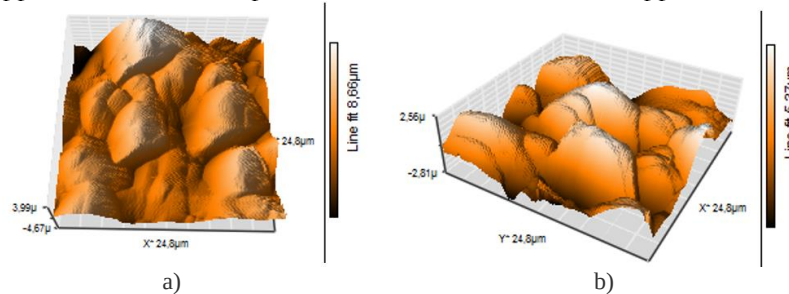


Fig. 13. 3D representations of the reference surface of S2: position 1 (a) and position 2 (b).

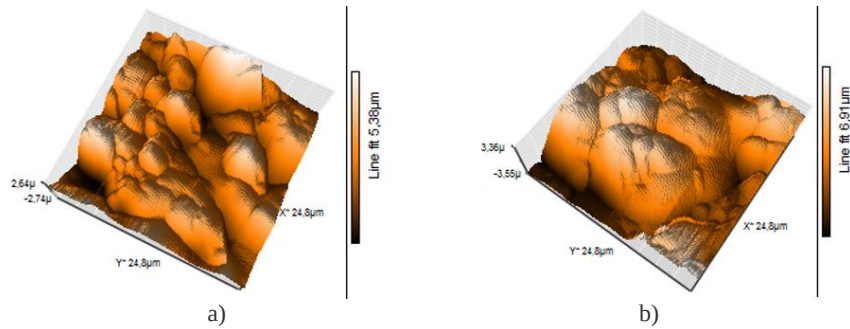


Fig. 14. 3D representations of thermal shock area no.4 from S2: position 1 (a) and position 2. (b).  
Table 5. Roughness average values of the AFM scanned surfaces, from sample 2.

| Sample                                                           | Area [μm <sup>2</sup> ] | Sa [nm] | Sq [nm] | Sm [μm] |
|------------------------------------------------------------------|-------------------------|---------|---------|---------|
| <b>S2 (Cr<sub>2</sub>O<sub>3</sub> + 10 wt% TiO<sub>2</sub>)</b> |                         |         |         |         |
| <b>Reference (1)</b>                                             | 618                     | 1075.3  | 1368.4  | 276.91  |
| <b>Reference (2)</b>                                             | 618                     | 868.41  | 1069.5  | 426.23  |
| <b>800°C, 9 cycles x 10 sec (1)</b>                              | 618                     | 1190.9  | 1432.2  | 56.942  |
| <b>800°C, 9 cycles x 10 sec (2)</b>                              | 618                     | 705.13  | 884.15  | 202     |

#### 4. Conclusions

Thermal spraying is a versatile process and plays a key role in improving material performance and reducing long-term costs. With a wide range of applications and adaptability to diverse industries, this technology supports advances in energy efficiency and sustainability and is a critical component for modern technological and industrial development.

Morphological analysis of the coatings revealed no major defects on the surface or at the interface with the substrate, the overall appearance being uniform, without discontinuities or macro cracks.

The Ti element is mainly present in splat-type areas, which confirms the role of finishing the structure, i.e. increasing the ductility of the ceramic coatings of which TiO<sub>2</sub> powder is part, by increasing the degree of incorporation of semi-molten or non-molten particles and by increasing the adhesion between the splats formed during spraying.

In the thermal shock tests, it was observed that in none of the cases did the morphology of the coating change (local melting, oxidation with formation of oxide products, cracking) irrespective of the temperature or cycles applied.

There are no dramatic increases in oxygen percentages in any of the heat-affected areas compared to the reference areas, so there is no additional oxidation of the coating regardless of the temperature at which it was heated.

When comparing the roughness of the areas on each sample with the reference surface, no relevant changes in roughness are observed. Also, when comparing the 2 types of coatings, it is observed that Ra increases slightly with increasing TiO<sub>2</sub> alloying percentage.

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